

New HTS superconductors + integrated high-B physics enable an innovative strategic vision for US leadership in accelerated fusion energy development



Gaps

G-8 High-B magnets

G-2 Integrated steady-state & boundary in burning plasma

G-4 Control at high Q_p

G-5 Predict & avoid damaging off-normal events

G-7 RF launchers & coupling

G-9 Tame PMI & heat exhaust

G-10-15 Integrated fusion materials & components

Next 10 years

HTS magnet R&D

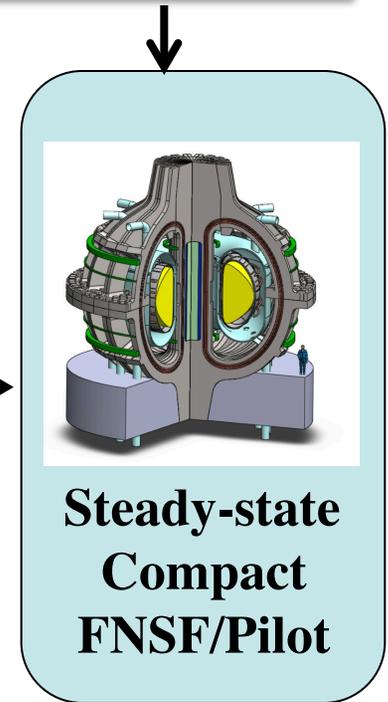
HTS high $B_{peak} > 20$ T Superconductor coils

High-B physics:

- High gain at small size
- Margin to operational limits & disruptions
- Effective RF CD & innovative launchers for steady-state
- High pressure boundary & PMI control

HTS joints & Blanket R&D

Demountable HTS coils & Modular replacement



A strategic plan should accelerate fusion development by considering critical knowledge gained in past decade



Key Observations

1. Large size → risks in cost and schedule

ITER successful fusion gain > 20 years away
“At some point delay is equivalent to failure”
*FESAC 2007 Gaps report*⁵

2. Superconductors evolved (G-8)

HTS^I tapes allow ~ double B field
→ Steady-state, high gain small devices

3. Boundary physics evolved (G-9)

- a) ELMs disallowed in ITER →
Transients disallowed in FNSF/Pilot/DEMO
- b) Power exhaust could threaten fusion viability
& does not favor large size.
- c) Quiescent high-field SOL → locate RF launchers

Evolved Strategy

Strategic
Input



**Small +
High-B +
Superconductor
=
Margin to
disruptions +
Steady-state +
Reduced cost
& schedule**

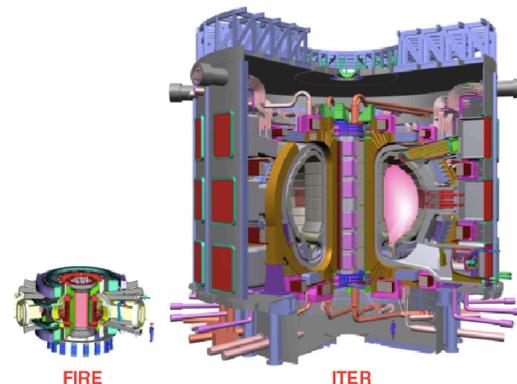


Size has risk: Lesson from fission & ITER

Minimize volume of first nuclear devices to assure timely development of physics and technology

<i>Design parameter</i>	Shippingport ² "Pilot" Fission Plant ca. 1954	ITER ³ "Pilot" Fusion Plant ca. 2006	Scale factor ITER/Shippingport
$P_{thermal}$ (MW)	236	500	x 2.5
Core volume (m ³)	60	~1600 (shield + TF)	x 27
Cost (2012 US B\$)	0.6	~ 30	x 50
Cost / Core volume (M\$/m³)	10	~ 18	~ 2
Construction time to "burn" (years)	3.3	~ 28	x 8

- JET ~ 100 m³ took < 5 years to construct
- FIRE B~10T burned at right size, but pulsed due to copper coils



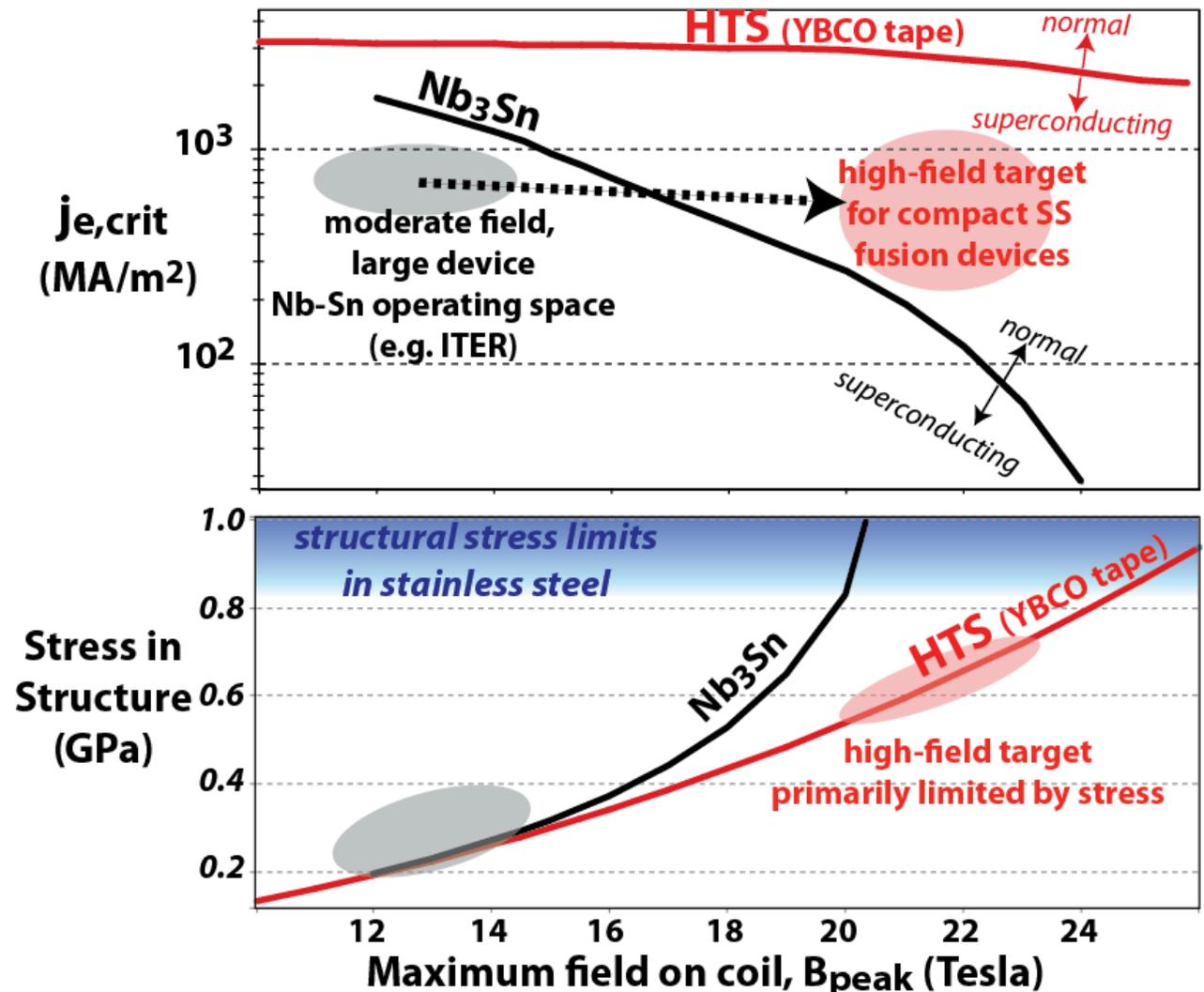
$$\frac{V_{FIRE}}{V_{ITER}} \sim \frac{1}{30}$$

Superconductors evolved

Astonishing critical current of new high-temperature superconductors (HTS) at $B_{\text{peak}} > 20$ T provides possibility to ~double loss-free B field



- Sub-cooled tapes at ~ 20 K provides operational margin to superconductor¹.
- Limitation becomes the structural stress rather than superconductor.
- Tapes allow joints.



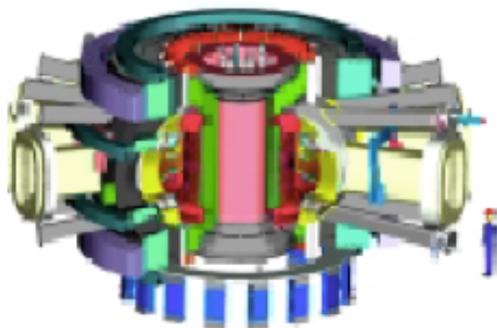
Cost &
schedule
G-2
G-4

Known physics scaling + Superconductor $B_{peak} > 20\text{ T}$ → High-gain burning plasma compact size & Steady state!



Gain $nT \tau_E \sim \frac{\beta_N H}{q_*^2} R^{1.3} B^3$ — $\$ \propto R^3$ — $\frac{P_{fusion}}{S_{wall}} \sim \frac{\beta_N^2 \epsilon^2}{q_*^2} RB^4$ **Power density**

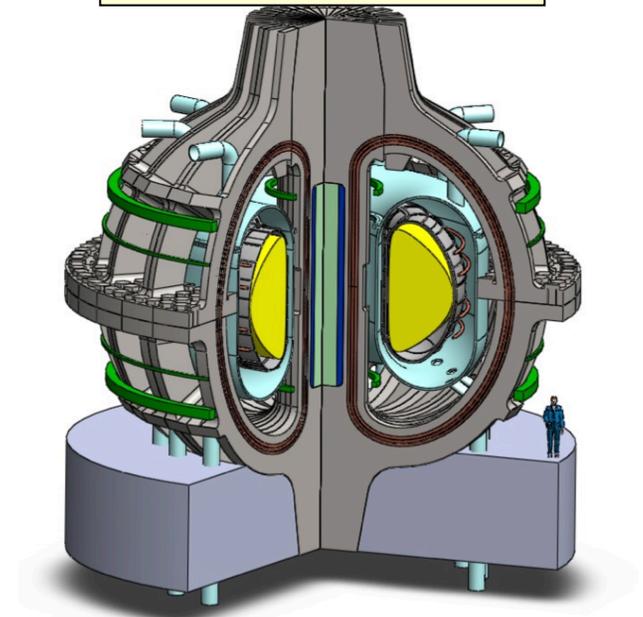
FIRE /w
copper coils



To scale

	FIRE ¹²	ARC ^{10,14}
R (m)	2.14	3.2
B ₀ (T)	10	9.2
Q _p	>10	>10
Steady-state	No	Yes
Tritium breeding	No	Yes
Q _{electric}	0	~4

ARC /w HTS
superconductor



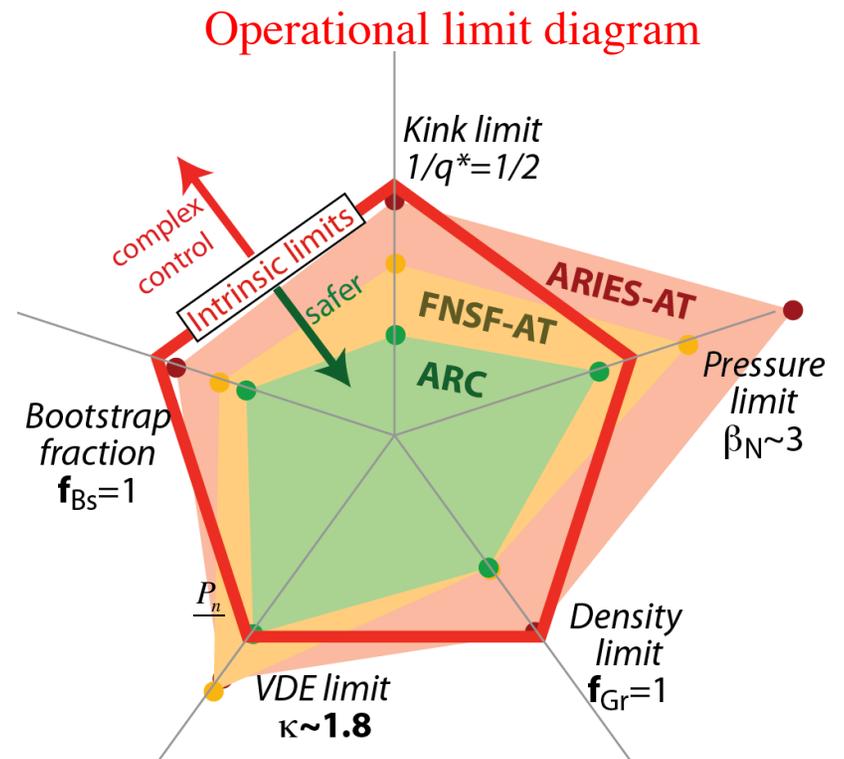


$B_0 \sim 10$ T, compact SC HTS tokamak enables more realistic high- Q_p steady-state option by providing margin to intrinsic disruption, control & operation limits

Capital & Operating Costs / Economics Nuclear mission Disruption damage relative to ITER

Steady-state tokamak	B_0 (T)	R (m)	P_{elec} (MW)	Q_p	$\frac{P_n}{S}$ $\frac{MW}{m^2}$	$\frac{W_{th}/S}{(W_{th}/S)_{ITER}}$
ARIES-AT ⁶ SC-NbSn	5.8	5.2	+1000	44	3.3	2.5
ARC ¹⁴ SC-HTS	9.2	3.3	+ 230	14	2.2	1.2
FNSF-AT ^{4,7} Copper	5.5	2.7	- 600	2.6	1.6	1

↓
Electrical cost¹³
~ 250-500 M\$/FPY



$$nT \tau_E \sim \frac{\beta_N H}{q_*^2} R^{1.3} B^3$$

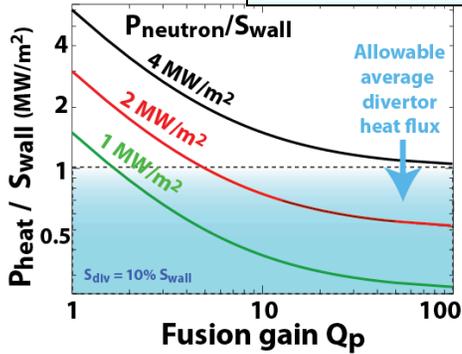
Heat exhaust critical to the viability of all FNSF/Pilot designs

New edge physics favors small size + high gain → high B



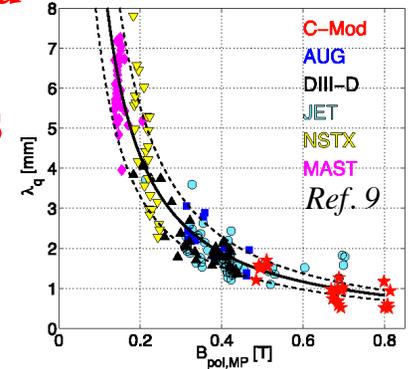
Neutron mission

$$P_{heat} \sim P_{neutron} \frac{(1 + 5/Q_p)}{4} \sim R^2$$



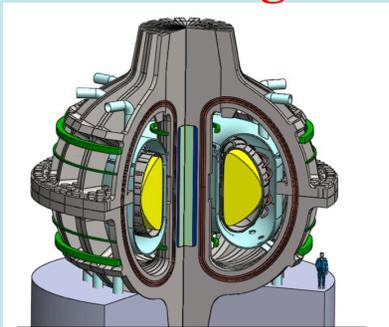
$$\lambda_q \sim \frac{1}{B_p}$$

Evolved edge physics



$$q_{||} \sim \frac{P_{heat} B}{R}$$

FNSF design challenge

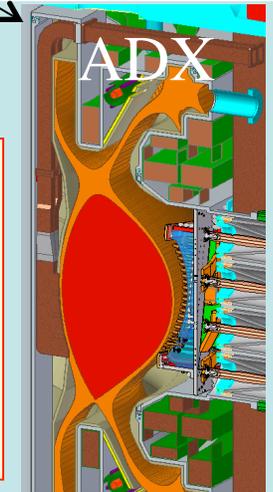


$$nT \tau_E \sim \frac{\beta_N H}{q_{95}^2} R^{1.3} B^3$$

$$q_{||} \sim R B (1 + 5/Q_p)$$

Near-term Edge physics

Innovative solutions at reactor-matched B, q//



LaBombard

US Leadership opportunity

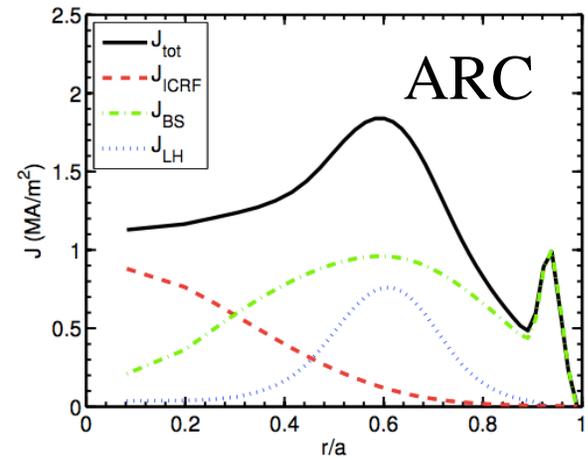
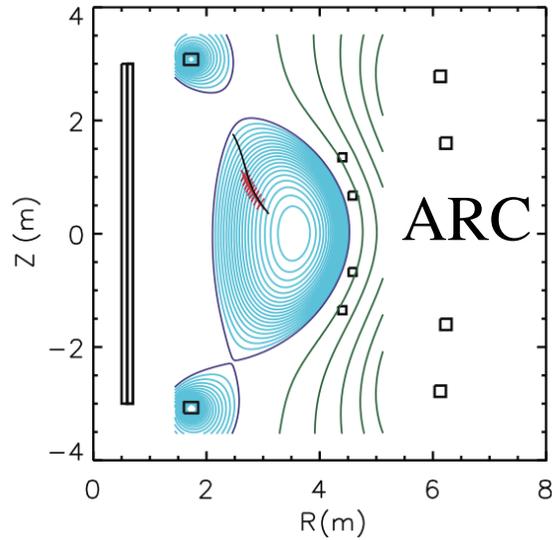
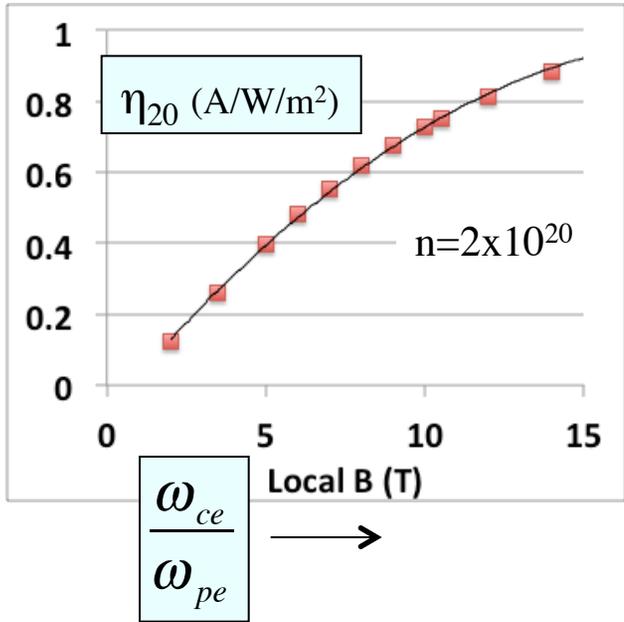
Efficient RF current drive is synergistic with high-B & critical to developing robust steady-state in tokamaks



Higher LHCD efficiency at high field

Quiescent PMI high-field-side RF launchers

Control current profile at small R, T~12 keV for optimized AT^{13,14}



$I_{CD}/I \sim 37\%$ & $Q_p \sim 15$

- Compels near-term research in high-field & inside launch RF. R. Parker

US Leadership opportunity

G-8
G-10
G-13
G-15



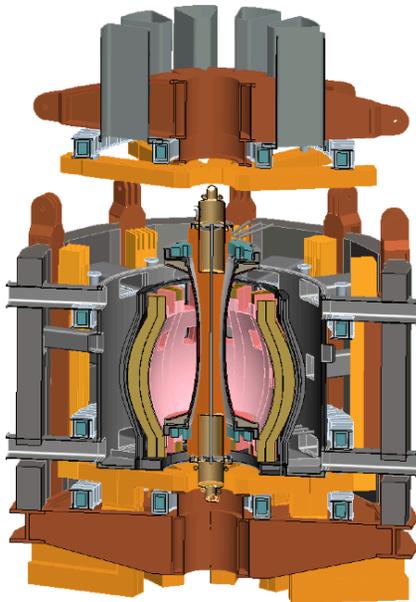
FNSF mission favors demountable coils for modular replacement

Finite resistance HTS joints \rightarrow minimal $P_{\text{coil}} \rightarrow$ Pilot option

US Leadership opportunity in configuration & maintainability

Conceptual FNSF designs

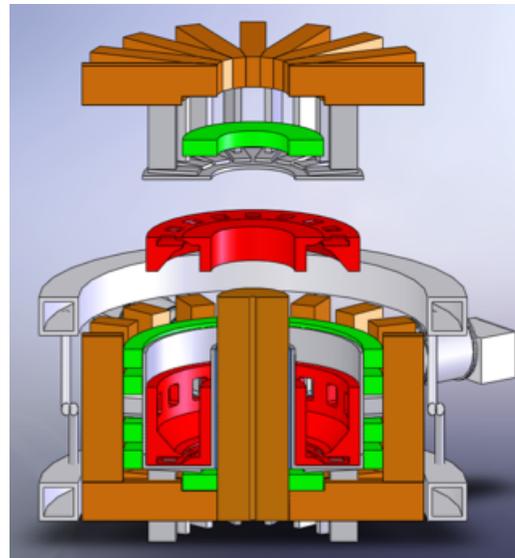
$R/a=1.7$



Copper FNSF-ST⁸

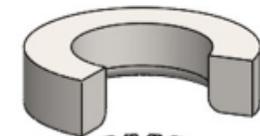
$P_{\text{coil}} \sim 400 \text{ MW}$

$R/a=3.5$

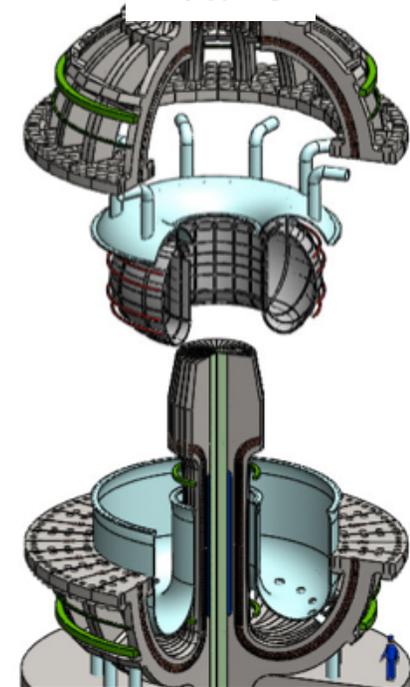


Copper FNSF-AT⁷

Coil $P_{\text{coil}} \sim 600 \text{ MW}$



$R/a=3$



**ARC: Resistive joints /w
HTS superconductors¹¹**

Coil $P_{\text{coil}} \sim 1 \text{ MW}$

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- G-10-15 Integrated fusion materials & components

Next 10 years

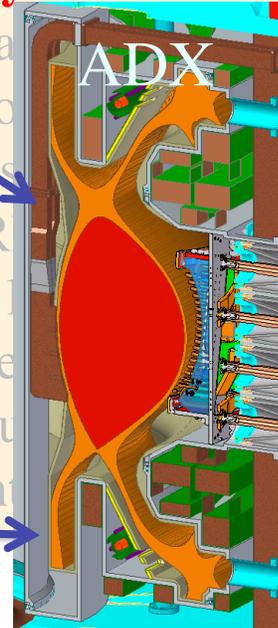
HTS magnet R&D

Minervini: HTS magnets

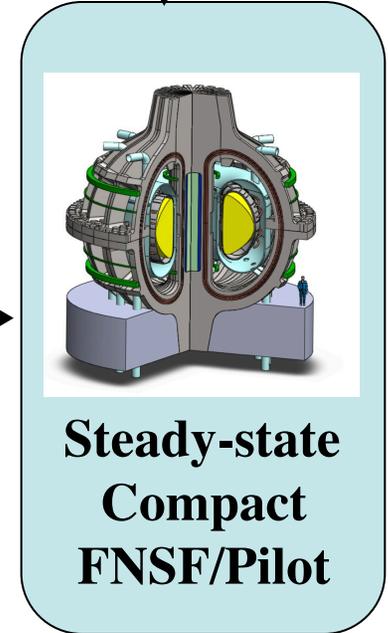
High-B physics:

Parker RF current drive

LaBombard PMI & heat exhaust



HTS high $B_{peak} > 20$ T Superconductor coils



HTS joints & Blanket R&D

Demountable HTS coils & Modular replacement

Backup materials



References



1. "Engineering critical current vs. applied magnetic field," P.J. LEE Florida State University, National High Magnetic Field Laboratory
<http://fs.magnet.fsu.edu/~lee/plot/plot.htm>
2. "Shippingport Atomic Power Station" Historic American Engineering Record, Dep. Interior, Philadelphia PA 19106 Report HAER No. PA-81
3. "ITER funding profile" <http://fire.pppl.gov/#NewsSection>, September 2012 US cost estimate of 3.1 B\$ as 9% partner.
ITER cost ~ 3.1 B\$ / 9% ~ 30 B\$
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5. "Priorities, Gaps and Opportunities: Towards a long-range strategic plan for magnetic fusion energy," FESAC report, M. Greenwald chair, Oct. 2007
6. F. Najmabadi, et al. "The ARIES-AT advanced tokamak, Advanced technology fusion power plant," Fus. Eng. Des. **80** 3 (2006).
7. A.M. Garofalo, et al. "A fast-track path to DEMO enabled by ITER and FNSF-AT," IAEA Fusion Energy Conference, **FTP/P7-35** San Diego, CA (2012) (Note: FNSF-AT version shown is with ECCD only)
8. J. Menard, et al. "Studies of ST-FNSF mission and performance dependence on device size," 1st IAEA DEMO Programme Workshop, UCLA, Los Angeles CA Oct. 2012
9. T. Eich et al Nucl. Fusion **53** 09031 (2013)
10. B. Sorbom, et al. " ARC: A compact, high-field disassemblable fusion nuclear science facility and demonstration power plant," being submitted to Fusion Engineering & Design (2014).
11. Z. S. Hartwig, et al., "An initial study of demountable high-temperature superconducting toroidal field magnets for the Vulcan tokamak conceptual design," Fusion Eng Design 87 (3), 201-214, 2012.
12. D. Meade, " Fusion, FIRE and and the Future," NRL seminar, December 2002 http://fire.pppl.gov/nrl_fire_120202.pdf
13. Electricity rate range: 50-100 \$/MW-hr x 8760 hr / Full-power Year x 600 MW = 262-525 M\$/FPY
14. D. Whyte, "Smaller & Sooner: Exploiting new superconductors for compact robustly steady-state tokamak reactor designs." JET/CCFE seminar, April 2014 http://fesac_2014.psfc.mit.edu/index.php/Main_Page#High-Field_Approach

National ADX and HTS magnet and ADX initiatives are aligned and timely to the OFES Burning Plasma Science mission

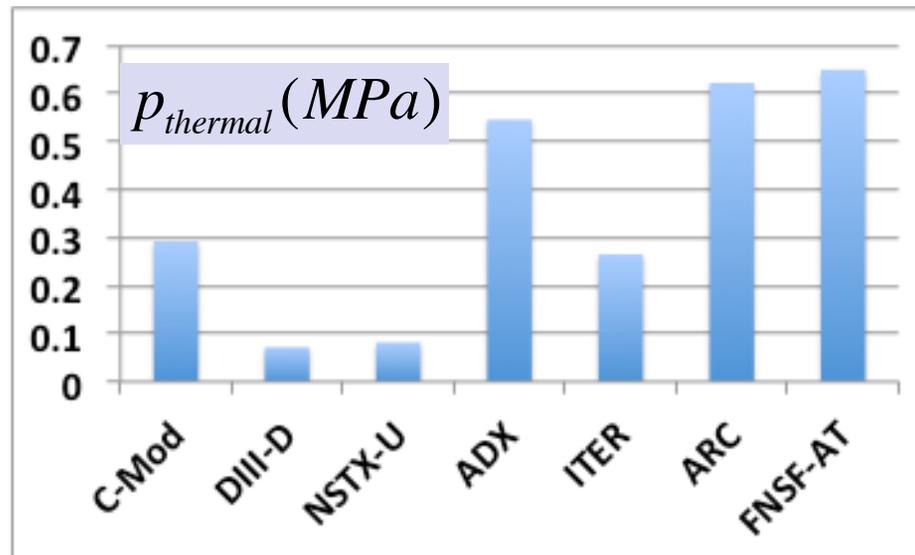
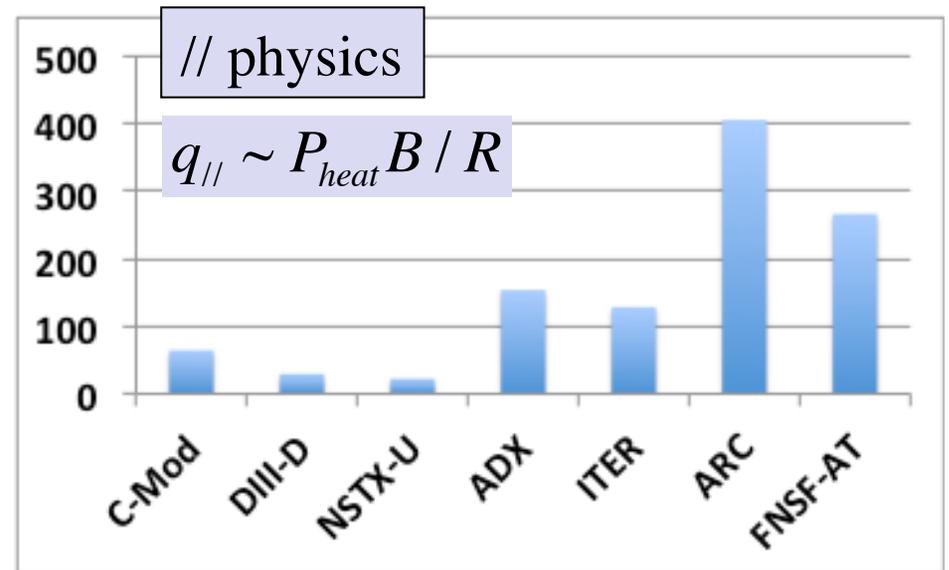
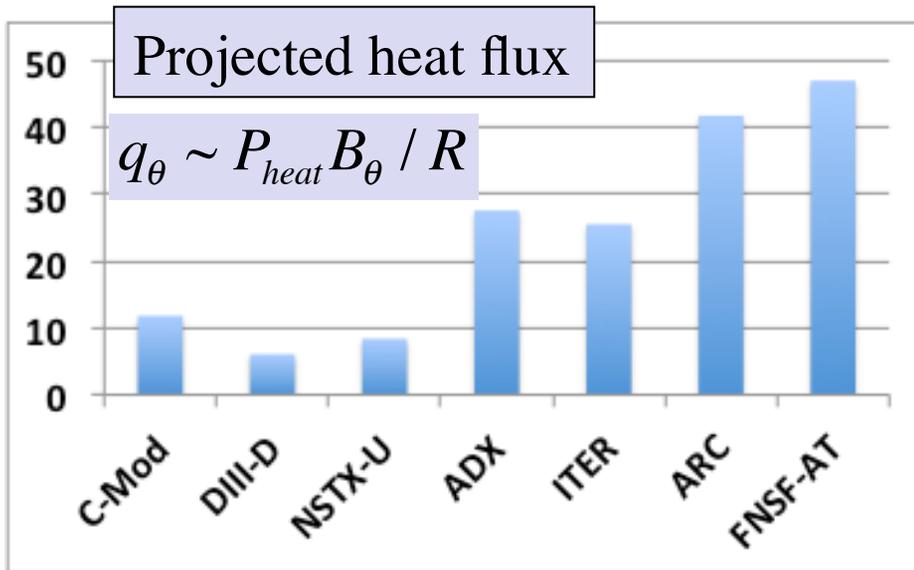


Foundations	Year 1-3	Year 4-7	Year 8-10	FNSF options
Transport		H ₉₈ OK, no X-point MARFE		Disruptivity vs. performance assessment
Stability			ELM-free stationary ped.	
Wave-particle	Design HFS launch: LHCD & ICRF	Install, assess PMI & coupling	High η_{CD} , j profile control	Valid RF model & launchers
PMI	Design divertors PMI diagnostics	Install divertors, q// vs. B physics	Integrated q// PMI solution @ high pressure	Heat exhaust/ PMI solutions Solid vs liquid
Long Pulse				
Plasma sustainment		CD efficiency f(B) on HFS	Disruption rates away from limits	Current control toolkit
B-field sustainment	Prototype HTS conductor & joints	Wound coils /w joints, HEP	B>20 T jointed coil demo	Cu vs. HTS Pilot?
Materials	Erosion resistance high-Z PFC	Study: modular replacement	High-T, high-Z, low E _{ion} divertor	Modular replacement

~17 M\$/y

~4 M\$/y + demo coil

ADX provides a critically needed near-term, small-scale step into the ITER/FNSF heat exhaust & PMI parameter range



Atomic & PMI physics

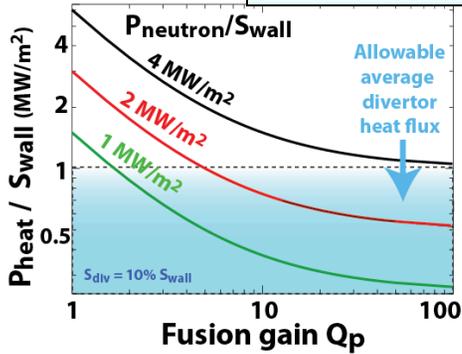
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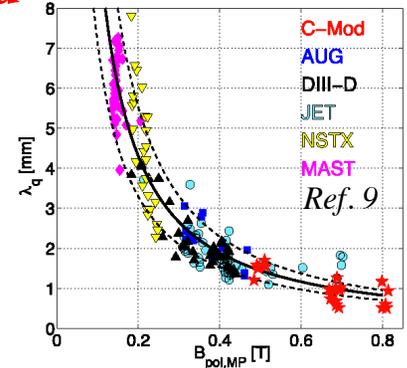
Neutron mission

$$P_{heat} \sim P_{neutron} \frac{(1 + 5/Q_p)}{4} \sim R^2$$



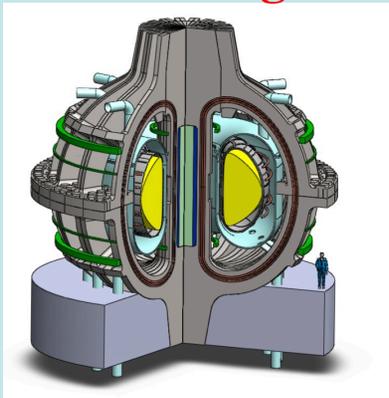
$$\lambda_q \sim \frac{1}{B_p}$$

Evolved edge physics



$$q_{||} \sim \frac{P_{heat} B}{R}$$

FNSF design challenge



$$q_{||} \sim R B (1 + 5/Q_p)$$

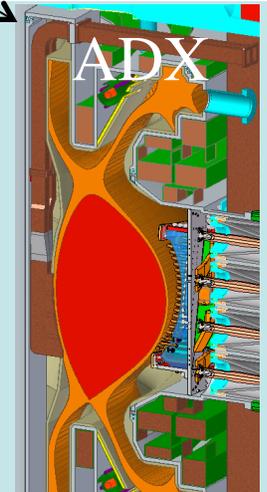
$$nT \tau_E \sim \frac{\beta_N H}{q_{95}^2} R^{1.3} B^3$$

$$q_{||} \sim \frac{(1 + 5/Q_p)}{B^{1.3}}$$

US Leadership opportunity

Near-term Edge physics

Innovative solutions at reactor-matched B, q//



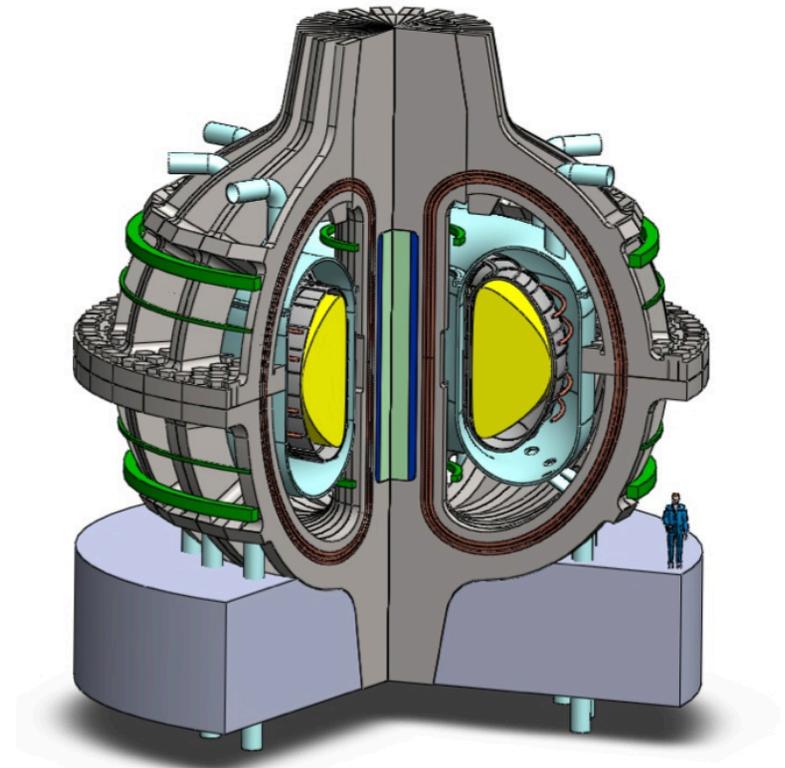
LaBombard

ARC: 9 Tesla “JET”, 250 MW net electricity

Steady-state tokamak far from disruptive limits

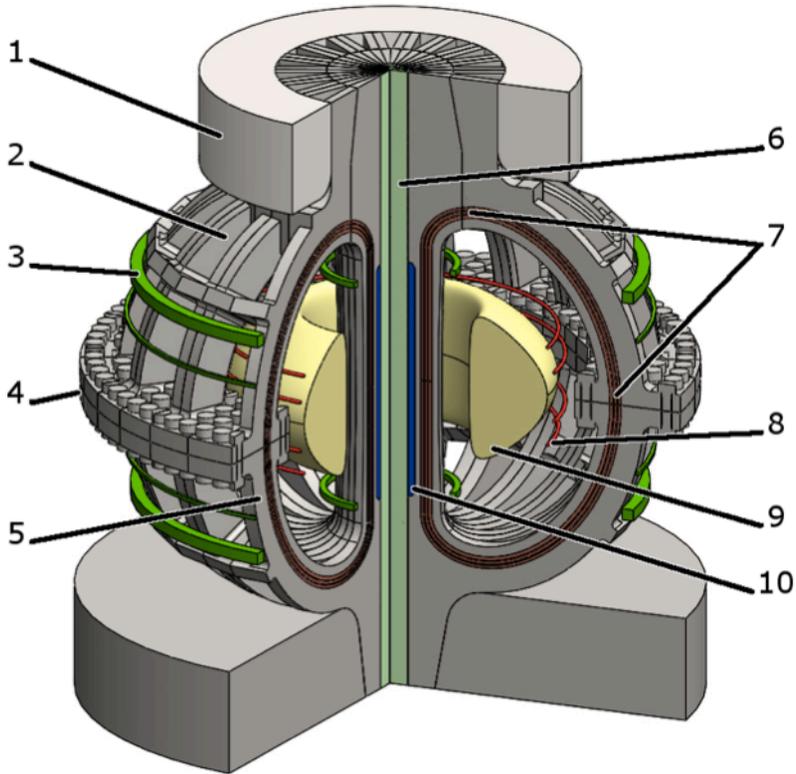


Nuclear	
Fusion Power	525 MW
Blanket & Depth	Liquid FLiBe > 0.8 m
$\eta_{\text{thermal}} / T_{\text{blanket}}$	$\sim 0.5 / \sim 900 \text{ K}$
Tritium breeding ratio	1.11
Plasma core	
$R / a / \kappa$	3.3 m / 1.1 m / 1.8
B_0	9.2 T
q_{95} / q_{min}	7.2 / ~ 3
β_N / H_{89}	2.59 / 2.7
$G_{89} : \beta_N H_{98} / q_{95}^2$	~ 0.15
Greenwald fraction	~ 0.6
RF current sustainment	
CD Efficiency	$> 0.4 \cdot 10^{20} \text{ A/W/m}^2$
Bootstrap fraction	63%



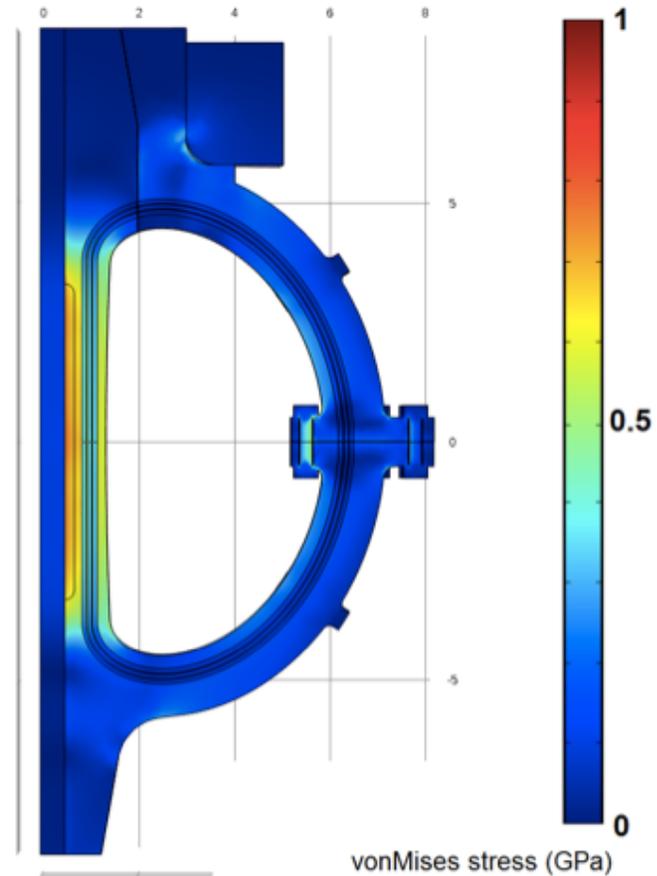
Margin to limits!
 Scenario already achieved
 In present tokamaks

ARC exploits two features of new SC: $B_{\text{coil,max}} \sim 23 \text{ T}$ + Tapes used for joints

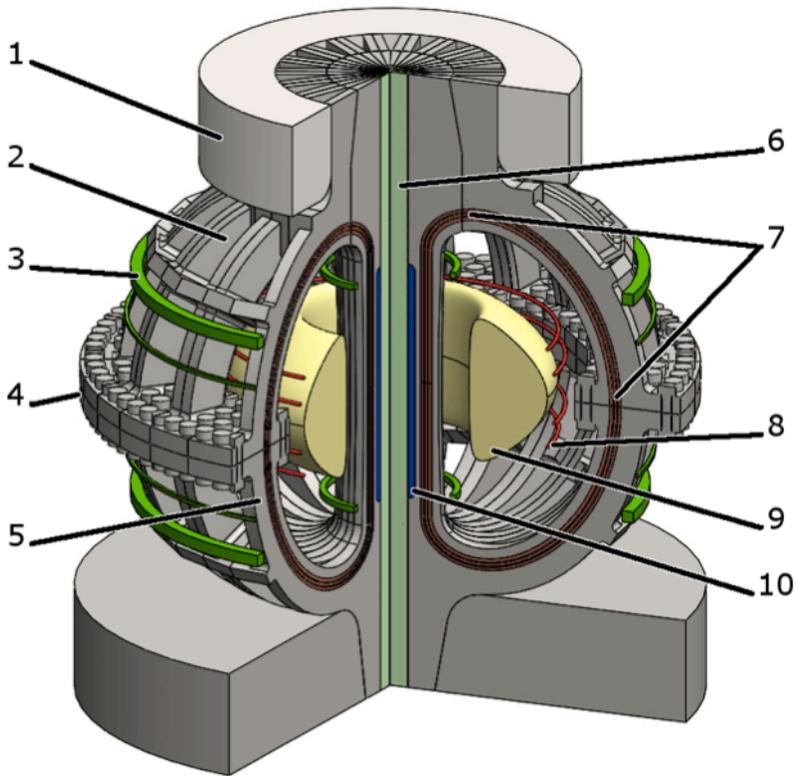


- 1. Support ring, 2. Top TF leg
- 4. Mechanical joint 6. Epoxy enforcement
- 7. Electrical joint

Peak stress $\sim 0.75 \text{ GPa}$
 $\sim 30\%$ margin for 316SS LN

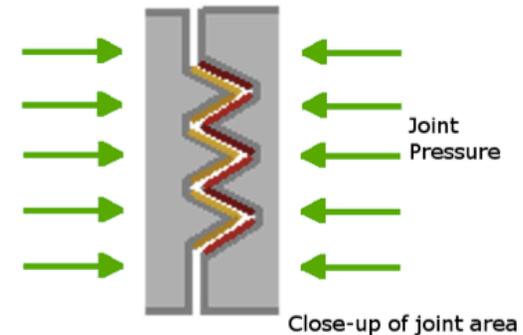
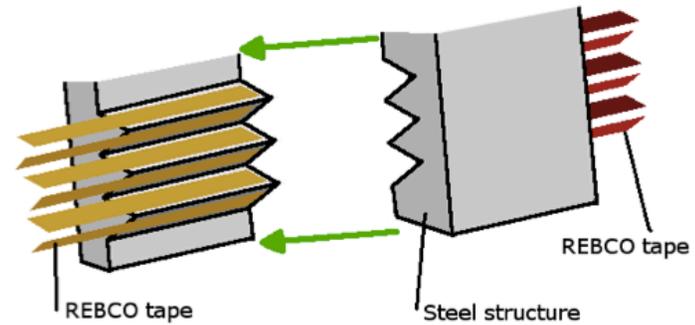


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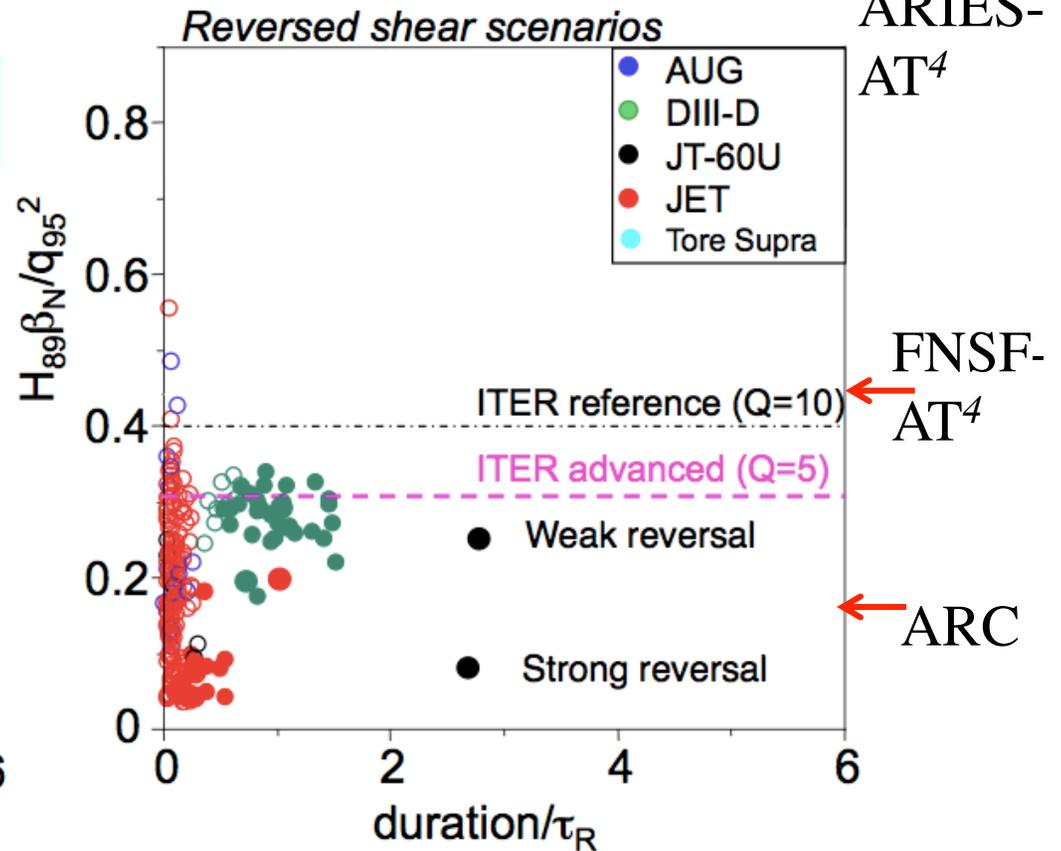
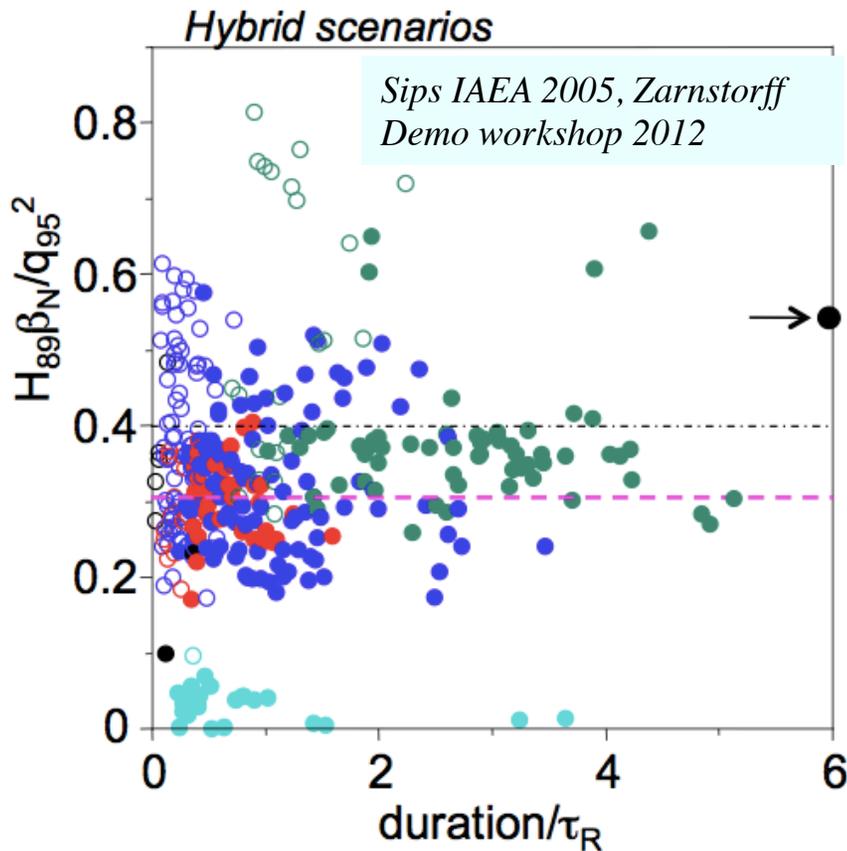


- 1. Support ring, 2. Top TF leg
- 4. Mechanical joint 6. Epoxy enforcement
- 7. Electrical joint

“Comb-style” TF resistive joints are expected to lead to $\sim 1 \text{ MW}_{\text{electric}}$ dissipation



HTS high-field allows FNSF/Pilot fusion & nuclear requirements with a modest integrated physics gain G_{89} already achieved in AT plasmas



$$nT \tau_E \sim \frac{\beta_N H}{q_{95}^2} R^{1.3} B^3$$



B~10 T, SC compact tokamak provides realistic high-gain steady-state option far from intrinsic operating and disruptive limits

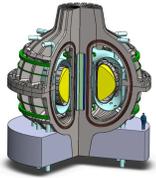
Steady-state tokamak	Capital & Operating Costs			Nuclear & Electricity		Power exhaust		Steady-state & Disruptions				
	B (T)	R (m)	P _{elec} (MW)	P _f (MW)	P _n / S (MWm ⁻²)	Q _p	P _{heat} / 4P _n	f _{BS}	κ	β _N	q*	f _{Gr}
ARC SC-HTS	9.2	3.3	230	525	2.2	14	1.3	0.63	1.8	2.6	4.8	0.65
ARIES -AT SC-NbSn	5.8	5.2	1000	1760	3.3	44	1.1	0.92	2.2	5.4	2.1	0.95
FNSF- AT Copper	5.5	2.7	-600	230	1.6	2.6	2.9	0.74	2.3	3.7	2.8	0.63

Electrical cost
~ 500 M\$/FPY

Q_p < 5 → excess relative
heat loading per neutron

Violation or within 10%
of intrinsic limits:

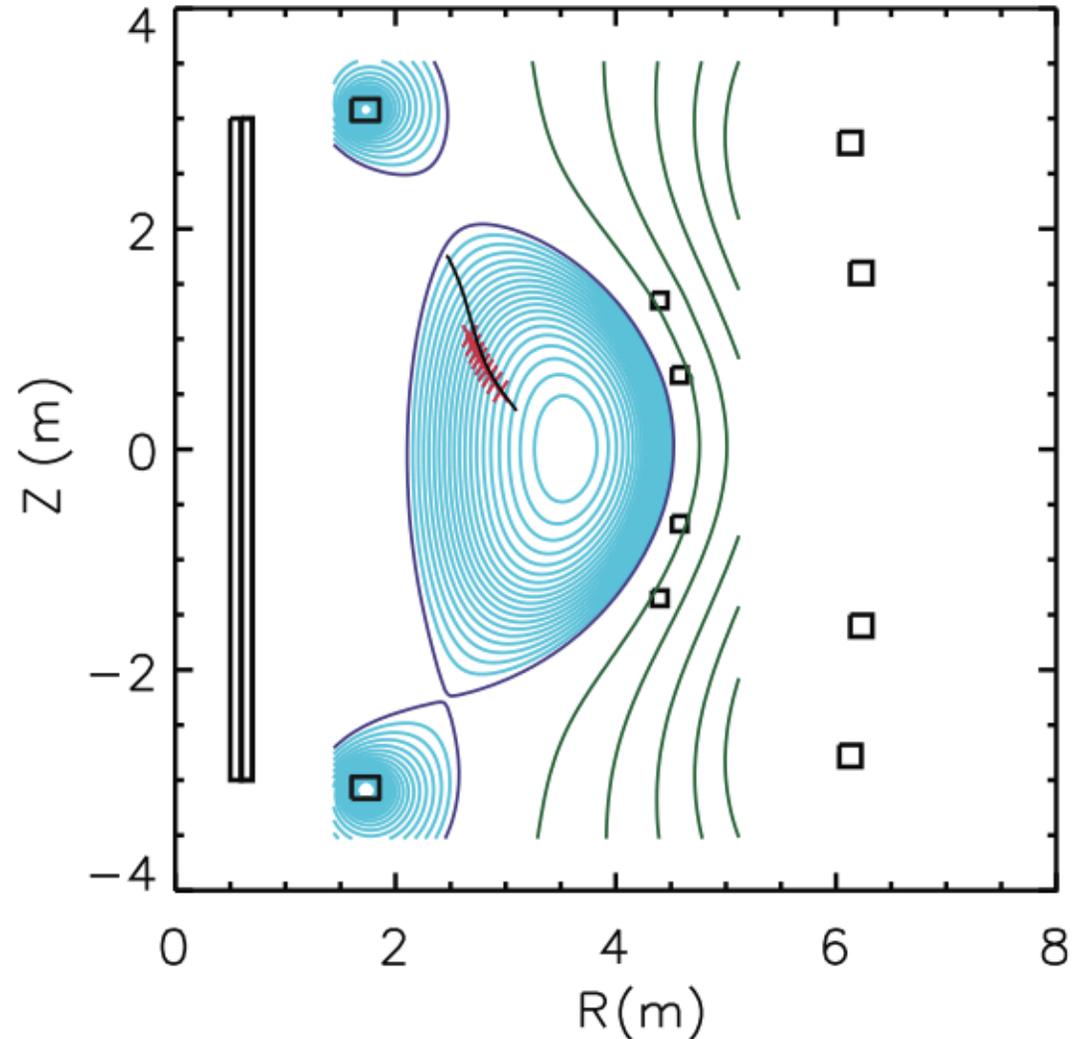
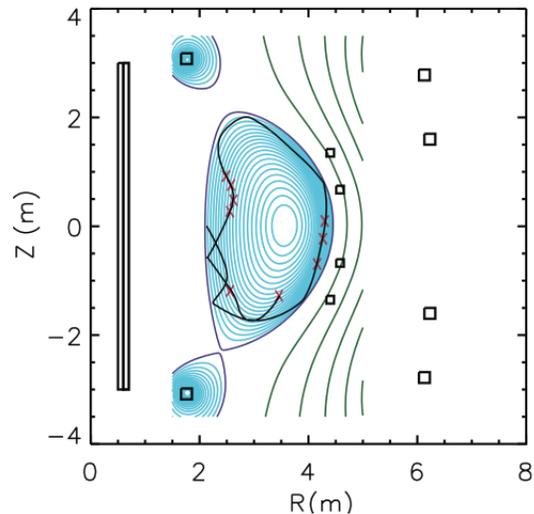
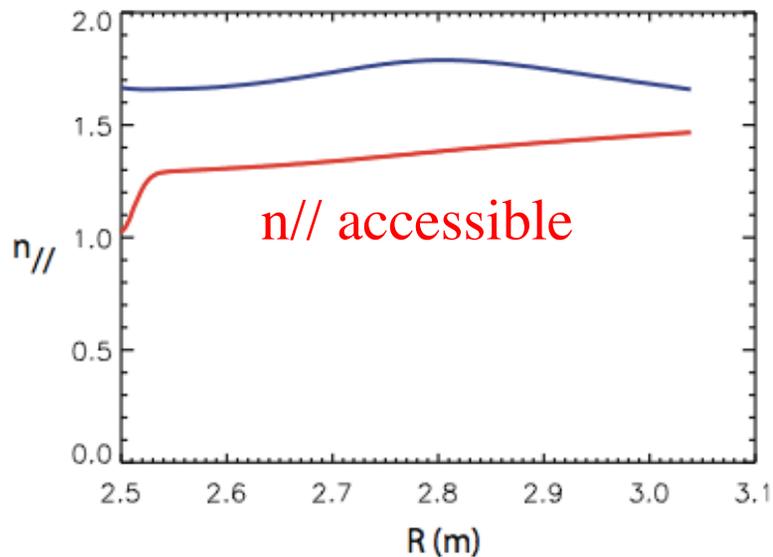
f_{bs}=1, κ < 5.4/A, no-wall β_N,
kink q*~2, density limit f_{Gr} =1

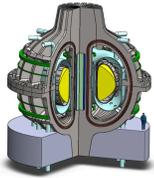


ACCOMME has optimized large advantages of HFS-LHCD + poloidal launch location near X-point

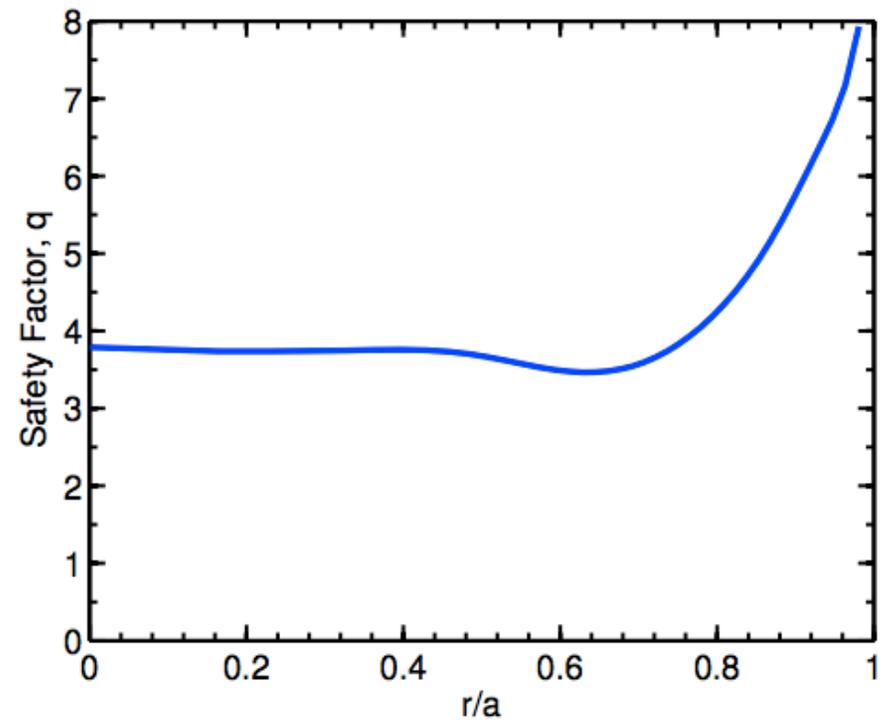
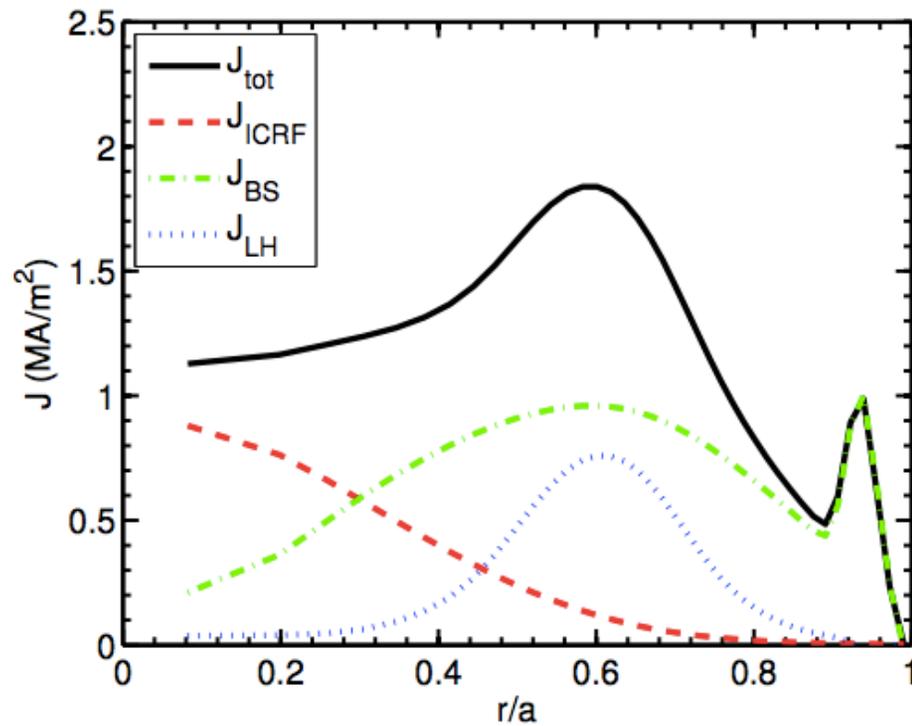


$n_{//}$ versus R

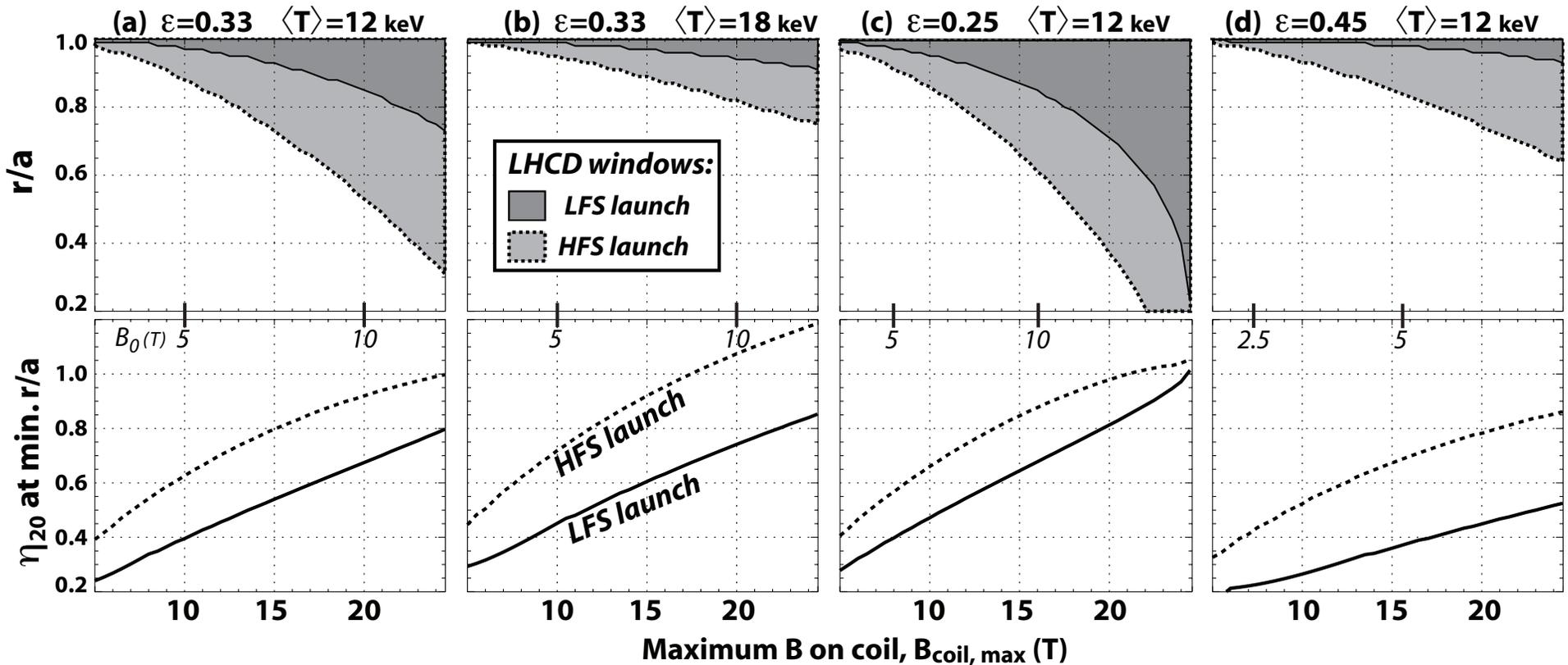




Optimized CD efficiency leads to substantial control of AT current profile below no-wall β_N limit



HFS-LHCD+ high B: Excellent penetration at Lawson criterion minimum $\langle T \rangle \sim 12$ keV, \sim doubled CD efficiency to standard scenarios

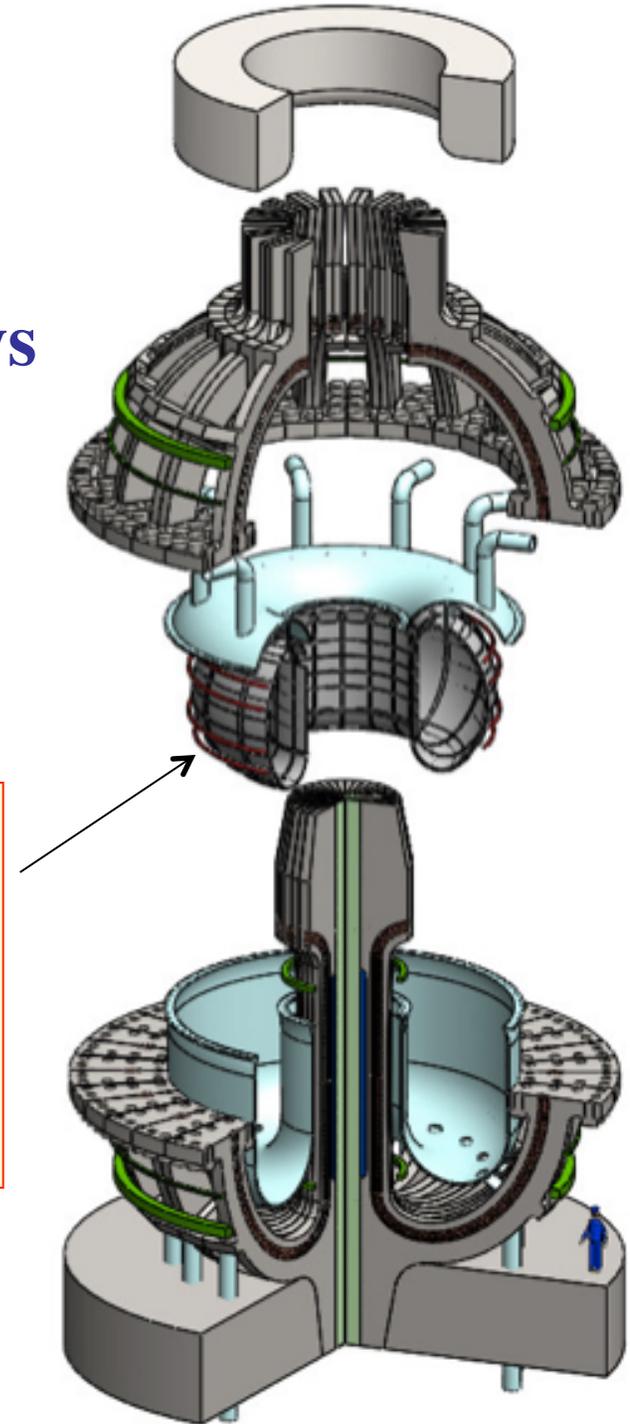


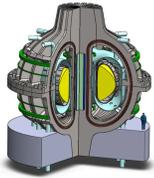
$p_{th} \sim 0.8$ MPa



Small scale + demounting has surprising synergistic benefits:
Reduced volume →
reduce cool/heat time to ~2-3 days
of structure
→ Modular maintenance

A single, module is only replaced unit
(vacuum vessel + PFCs +
Built-in test stations
integrated off-site)





Small scale → Modular VV → Low-risk immersion liquid blanket (FLiBe) for FNSF

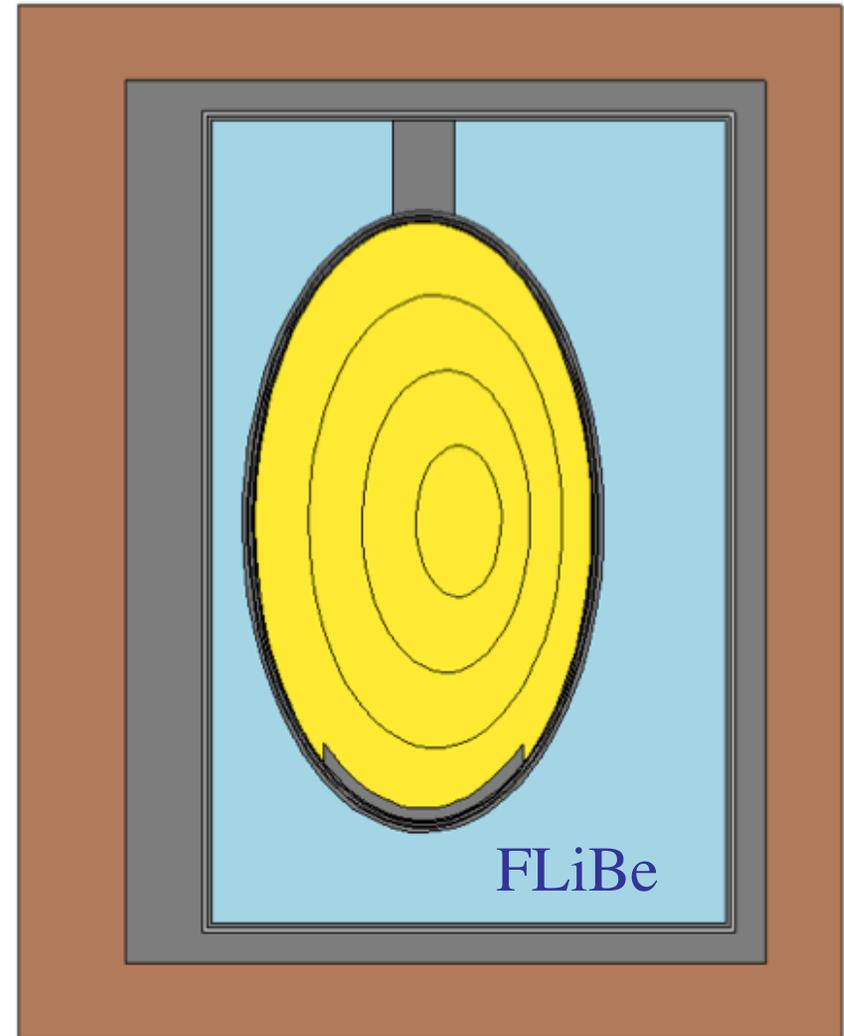


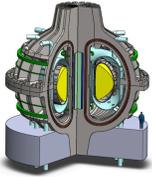
Property	FLiBe	Water
Melting Point (K)	732	273
Boiling Point (K)	1703	373
Density (kg/m ³)	1940	1000
Specific Heat (kJ/kg/K)	2.4	4.2
Thermal Conductivity (W/m/K)	1	0.58
Viscosity (mPa-s)	6	1

Tritium Breeding Ratio: 1.14

Eliminate blanket solid waste

No “blanket” DPA limit



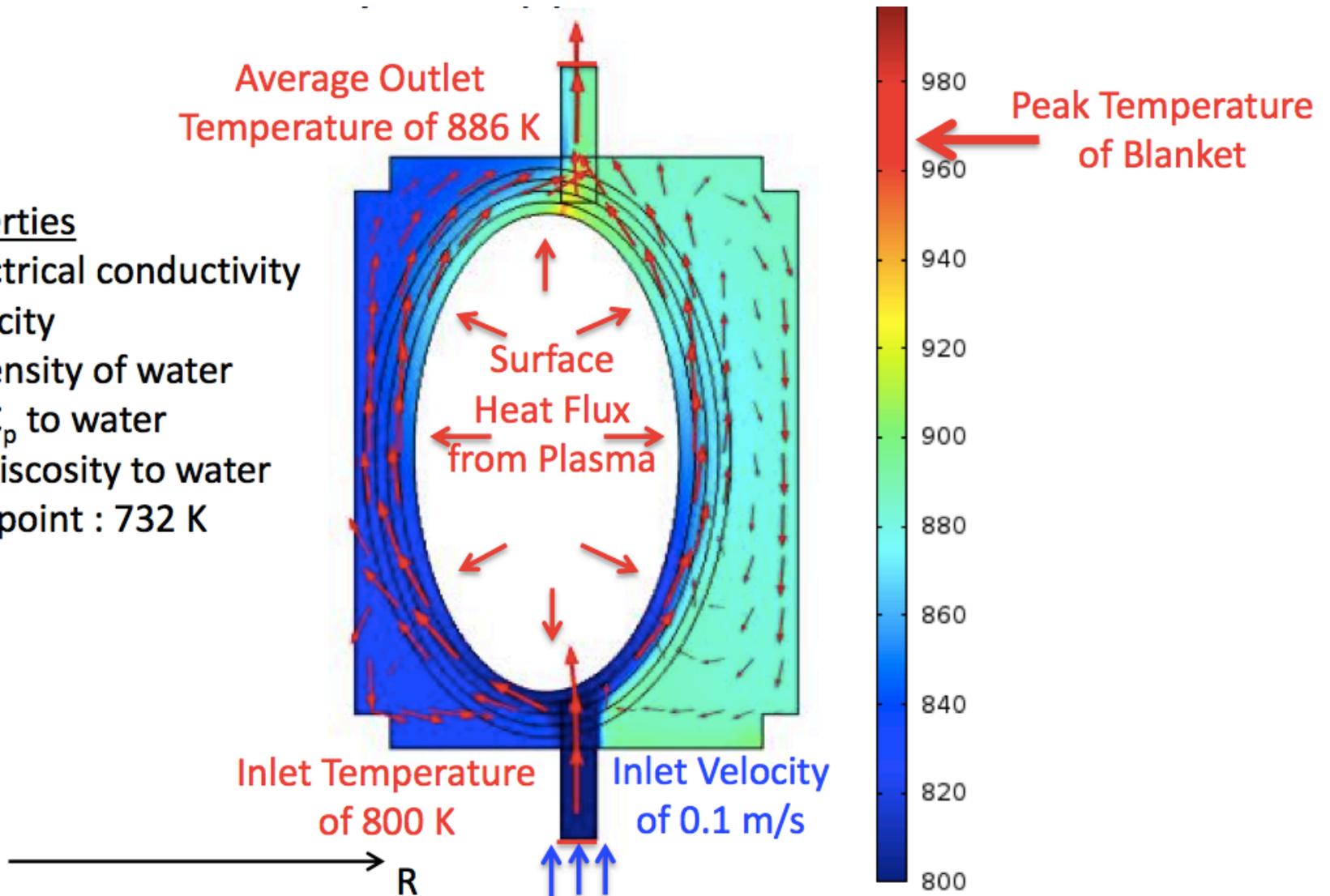


FLiBe provides outstanding heat removal capabilities at high T → thermal efficiency



FLiBe Properties

- Low electrical conductivity
- Low toxicity
- Twice density of water
- Similar C_p to water
- Similar viscosity to water
- Melting point : 732 K



Lessons from ARC..



- **Is NOT that ARC is the ultimate, best fusion reactor design..**
- **Or that every detail of ARC is settled and easily done...**
- **ARC and its innovations were the result of ~dozen MIT students working for a semester+ , showing that it was feasible to produce high gain, SS reactor at JET size**
- **The real lesson of ARC is that when you change the most fundamental aspects of your MAGNETIC fusion device, i.e. scale, B strength and coil configuration, you also fundamentally change the design options and solutions open to you...**